Erratum

Higher Mean-Flow Approximation for a Solid Rocket Motor with Radially Regressing Walls

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In N A recent study leading to an exact solution of the Navier–Stokes equations [1], a mistake in calculating a simple constant propagates into several equations. The error first appears in Eq. (29) of the subject paper, where the coefficient of the third derivative at order ε must be a "4" instead of a "3." To confirm this correction, we consider the case for which the porous walls are not regressing (i.e., $\alpha = 0$); in this context, we recognize the importance of recovering the model equation obtained by Yuan and Finkelstein [2], which is further confirmed by Terrill and Thomas [3]. This will be the case only when the proper constant 4 is used. In what follows, each equation affected by this oversight is listed in its amended form. Note that graphical results in [1] remain accurate representations of the solution because of the small discrepancy that this change brings to bear on the model.

$$\varepsilon \left[2\eta \frac{\mathrm{d}^4 F}{\mathrm{d}\eta^4} + (2\alpha\eta + 4) \frac{\mathrm{d}^3 F}{\mathrm{d}\eta^3} + 4\alpha \frac{\mathrm{d}^2 F}{\mathrm{d}\eta^2} \right] + F \frac{\mathrm{d}^3 F}{\mathrm{d}\eta^3} - \frac{\mathrm{d}F}{\mathrm{d}\eta} \frac{\mathrm{d}^2 F}{\mathrm{d}\eta^2} = 0$$
(29)

$$\sin \theta \frac{d^3 F_1}{d\theta^3} - \cos \theta \frac{d^2 F_1}{d\theta^2} + \sin \theta \frac{d F_1}{d\theta} - \cos \theta F_1$$

$$= \left(\frac{2}{\pi} \alpha \theta + 4\right) \cos \theta + \frac{4}{\pi} \alpha \sin \theta - 2\theta \sin \theta \tag{32}$$

$$-K_0'\sin^2\theta - K_1'(2\sin^2\theta + \theta\cos\theta\sin\theta) - K_2'\cos\theta\sin\theta$$
$$= [(2\alpha/\pi)\theta + 4]\cos\theta + (4\alpha/\pi)\sin\theta - 2\theta\sin\theta \tag{39}$$

$$K_0 = (\alpha/\pi)[-\theta \csc \theta + 3 \ln \tan \frac{1}{2}\theta + (\cos \theta - \theta \sin \theta)]$$
$$-2 \csc \theta - \sin \theta - \theta \cos \theta - S(\theta) + C_0$$
(40)

$$K_1 = (\alpha/\pi)(\theta \csc \theta - 3 \ln \tan \frac{1}{2}\theta) + 2 \csc \theta + S(\theta) + C_1$$
 (41)

$$K_2 = (\alpha/\pi)[3S(\theta) - \theta\cos\theta - \sin\theta - \theta^2\csc\theta]$$
$$-\cos\theta + \theta\sin\theta - 2\theta\csc\theta - S_1(\theta) + C_2 \tag{42}$$

$$F = \sin \theta + \varepsilon \{ (\alpha/\pi) [3(\sin \theta - \theta \cos \theta) \ln(\tan \frac{1}{2}\theta) - 2\theta]$$

$$-3 + (\theta \cos \theta - \sin \theta) S(\theta) + [3(\alpha/\pi) S(\theta) - S_1(\theta)] \cos \theta$$

$$+ C_0 \sin \theta + C_1 \theta \cos \theta + C_2 \cos \theta \}$$
(45)

$$C_1 = -6/\pi + 2\alpha/\pi^2 - 1 - S(\frac{1}{2}\pi)(6\alpha/\pi^2 + 1) + (2/\pi)S_1(\frac{1}{2}\pi)$$
(46)

$$C_0 = \alpha + 3 + S(\frac{1}{2}\pi), \qquad C_2 = 3$$
 (47)

$$P_{\eta} = -[\varepsilon F_{\eta} + \alpha \varepsilon F + \eta^{-1} (F/2)^{2}]_{\eta}$$
 (50)

$$\Delta p_z \equiv p(\eta, z) - p(\eta, 0)$$

$$= \frac{1}{2} z^2 \{ \varepsilon [2\eta F_{\eta\eta\eta} + 2(1 + \alpha\eta) F_{\eta\eta} + 2\alpha F_{\eta}] + F F_{\eta\eta} - (F_{\eta})^2 \}$$
(52)

References

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